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MEMS Piston Mirror Arrays for Computer Generated Holography

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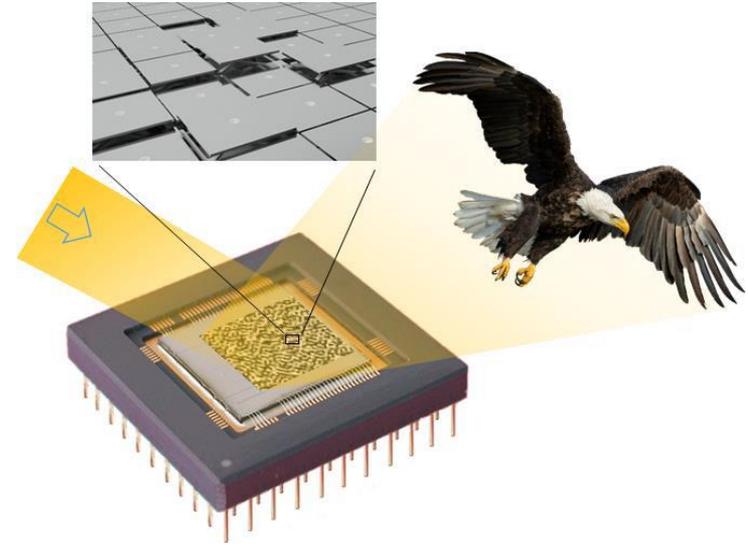
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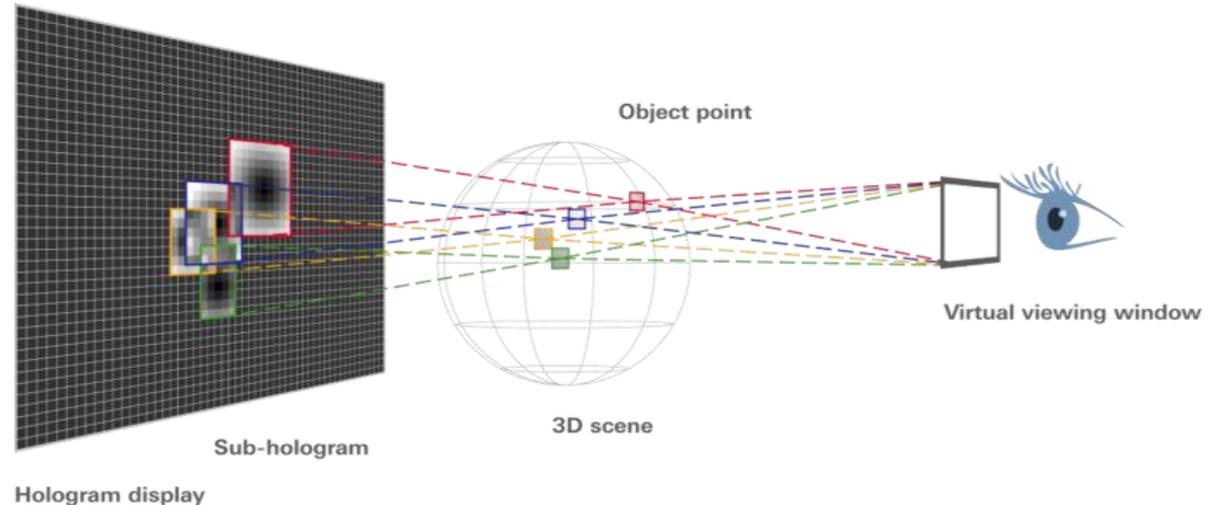
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Introduction

- holographic displays have been a fascinating prospect for a long time
- only real holography can provide a fully natural viewing experience
- the data volume is generally prohibitively huge
- due to the progress in computer power and by restriction to small viewing windows real holographic displays are now becoming feasible
- SLMs remain a challenge

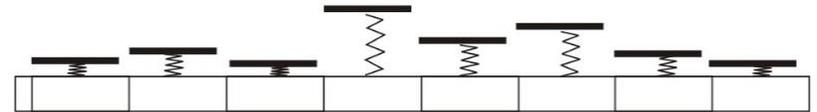


Challenges for SLMs in Holography

- very many pixels
- pixels as small as possible for large diffraction angle (→ low drive voltage)
- phase modulation is better than intensity modulation
- analogue modulation of light
 - binary modulation is inferior, pulse width modulation not feasible

→ DLP-SLMs are sub-optimal

- high frame rates
- high precision, stable deflection, low cross-talk

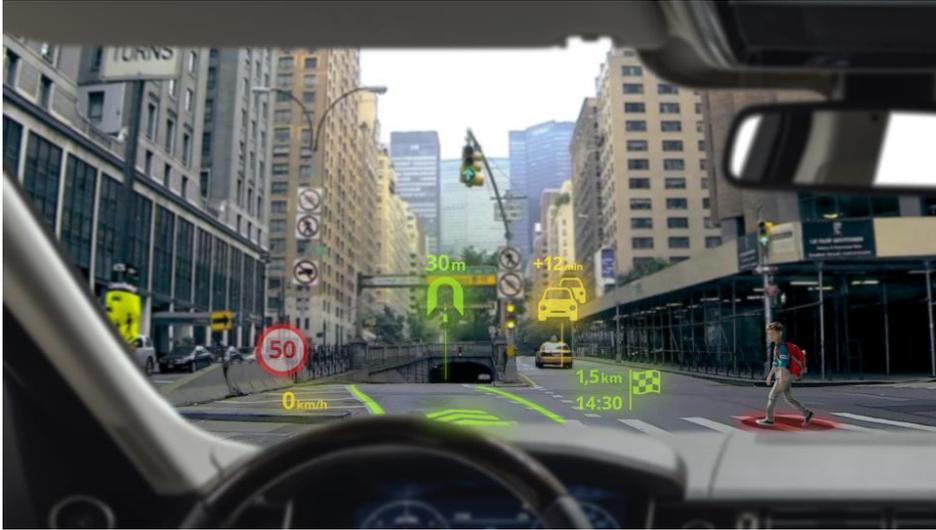


→ LCoS-SLMs are sub-optimal

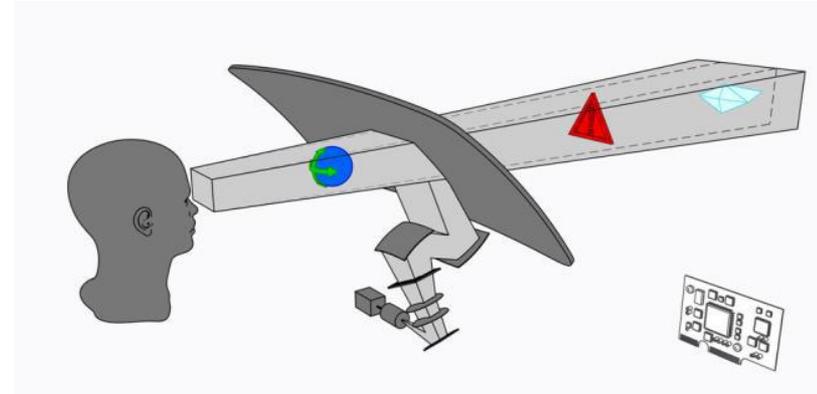
- micro mirrors work independent from polarization
- low power dissipation

→ analogue piston mirror SLMs are perfect for holography, but development is needed

Application Example: Automotive 3D Head-up Display



- Marking of potential risks
- Lane guidance
- Vehicle data
- Additional traffic signs

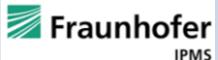


Added value over conventional HUD

- Information is displayed with correct spatial 3D placement, updated in real time
- No eye fatigue or misperception
- Real driver assistance, not distraction

RealHolo Project Consortium

EU Horizon 2020 Project 'REALHOLO', Project duration: Jan. 2021 ... Dec. 2024

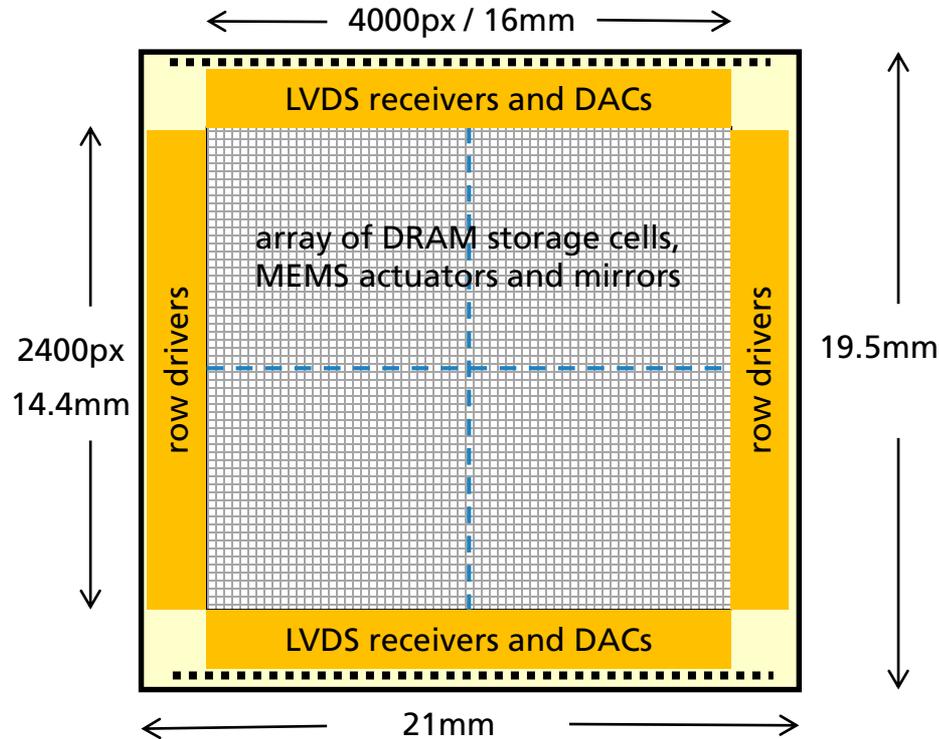
partner	country	task
	AT	management
	DE	system development
	DE	MMA development
	BE	CMOS design
	PL	addressing electronics
	FR	display demonstrator
	NL	packaging
	FR	CMOS backplane

The **REALHOLO** project receives funding from the European Union's Horizon 2020 research and innovation programme under grant agreement 101014977.

This project is an initiative of the Photonics Public Private Partnership.

<https://realholo.eu>

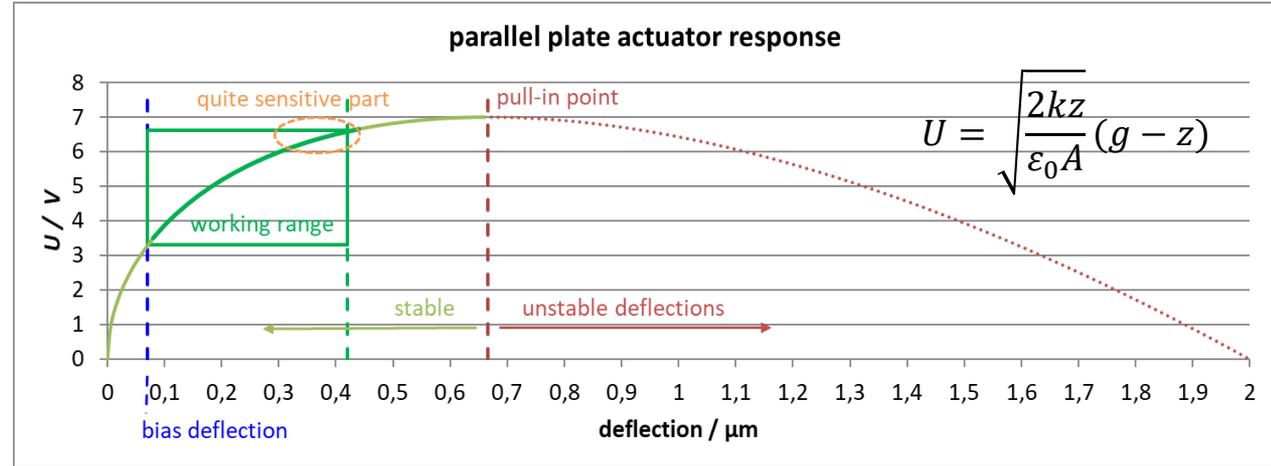
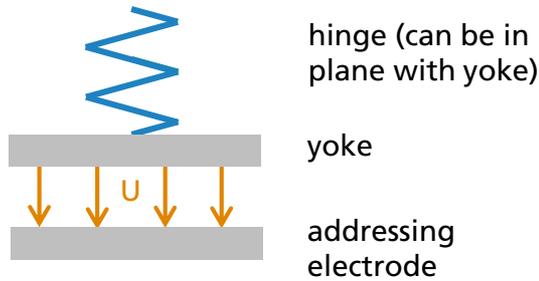
RealHolo MMA Key Parameters



Parameter	Target
pixel size	4 μ m x 6 μ m
pixel count	4000 x 2400
active area	16mm x 14.4mm
vertical deflection	0 ... 350nm
tilt error	< 0.1° (< 1.75mrad)
frequency	> 1kHz
duty cycle	> 20%
power consumption	< 2.5W
pixel voltage	0V to 3.3V
deflection precision	8bit

- the pixel area is divided into 4 subareas which are addressed from the edges

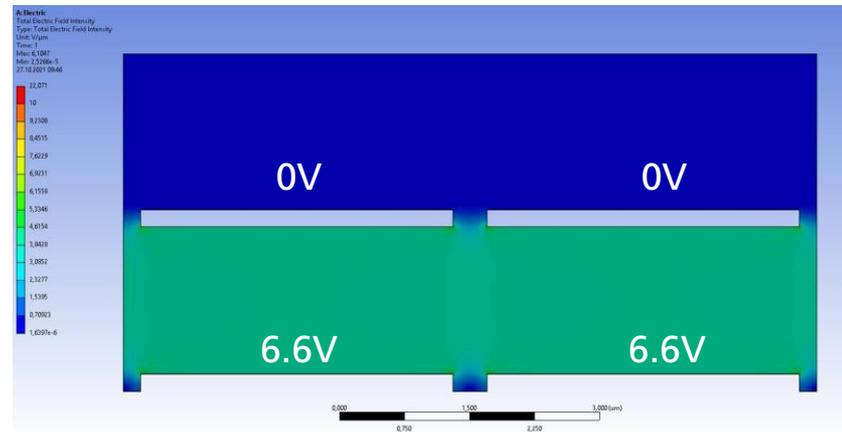
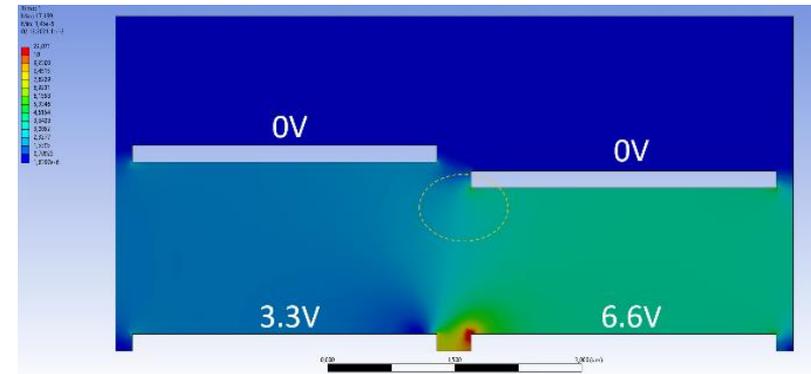
Parallel-Plate Actuators Need Large Actuator Gaps



- Analytical model with linear spring and plate capacitor
- Force equilibrium between mechanical force $F_m = -k \cdot z$ and electrostatic force $F_{el} = \frac{\epsilon_0 A U^2}{2(g - z)^2}$
- Force equilibrium can be solved analytically for deflection curve
- Electrostatic pull-in happens at gap/3
- a maximum deflection of about 60% of the pull-in deflection or 20% of the gap can be used

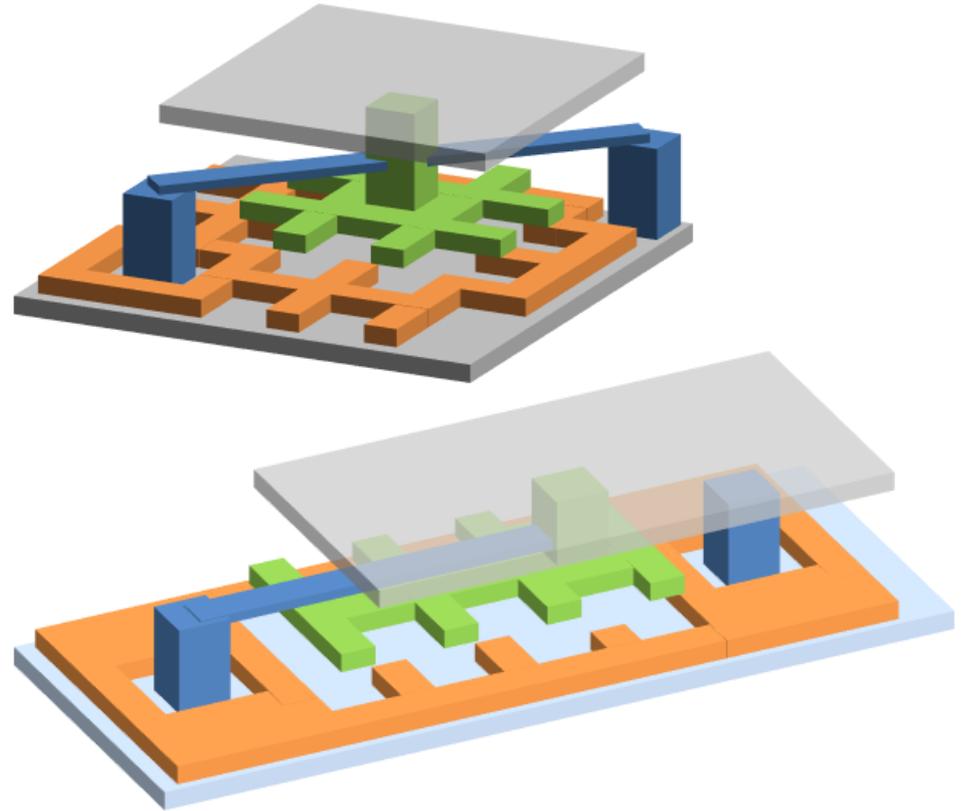
Parallel-Plate Actuators

- deflection needs to be $\lambda/2 \approx 350\text{nm}$ for red light
- the actuator gap needs to be about $2\mu\text{m}$, which is only twice the pixel width
- due to the large gap the total electrostatic force is small: $\sim 1.5\text{nN}$
- and the electrostatic cross-talk is large
 - simulated cross-talk of $\sim 3.5\%$ at one edge
 - would be $\sim 14\%$ for 4 neighbor pixels



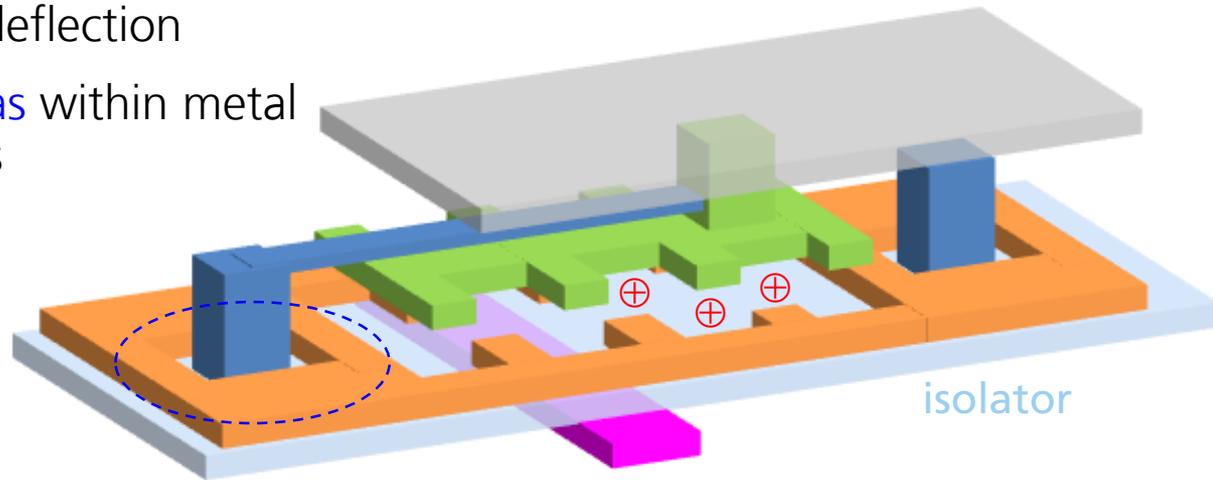
Novel Comb Drive Actuator Concept

- comb-drive actuators have no pull-in effect (in direction of intended deflection)
- the actuator gap may be very small
→ ~10x larger electrostatic forces in spite of electrode small area
- the cross-talk may be very small due to the concentrated electrostatic field around the fingers
- a one-sided hinge allows for compliant, linear behavior and can still produce tilt-free deflection



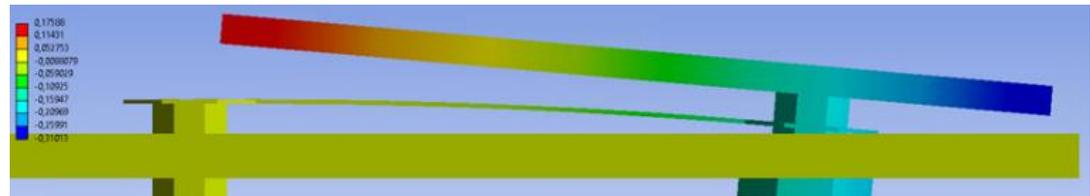
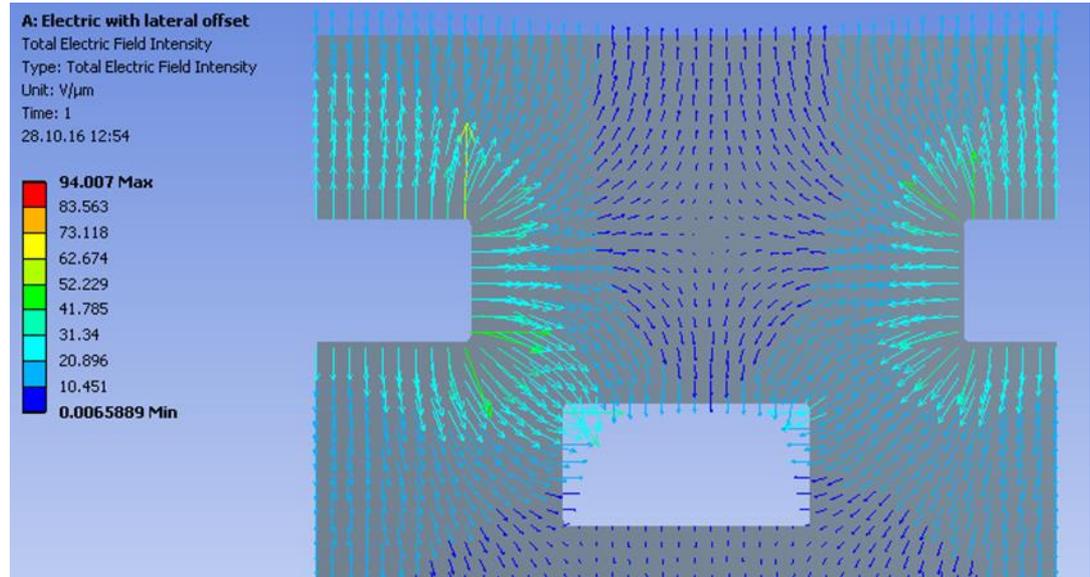
Possible Issues with the Comb Drive Actuator (I)

- the **underlying circuitry** may directly attract the yoke
 - deviation from desired deflection
 - an electrical shield could again cause pull-in
- isolators may have **trapped charges**
 - deviation from desired deflection
- small defects in **critical areas** within metal layers may cause short cuts
 - pixel defect
- small area for connection MEMS to backplane
- high aspect ratio posts are difficult to fabricate



Possible Issues with the Comb Drive Actuator (II)

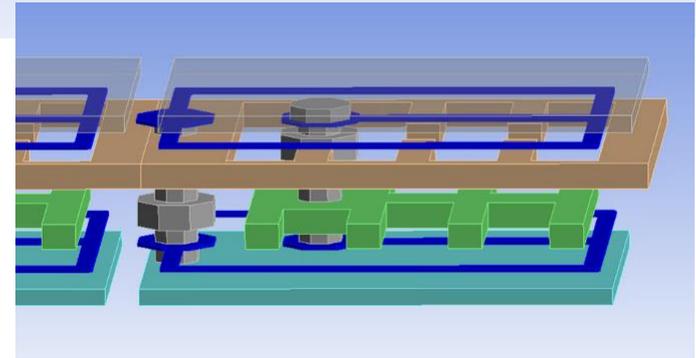
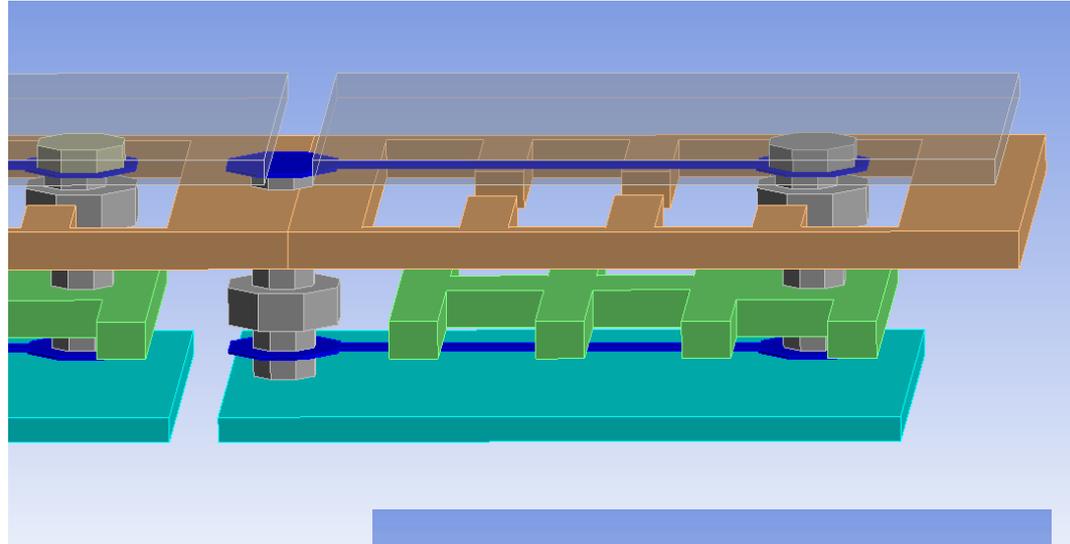
- an overlay error or other asymmetry of the combs causes large horizontal forces and an imbalance of the vertical forces
→ tilting mirror or even horizontal pull-in
- even small stress gradients in the hinge cause strongly tilted actuators, here 100MPa → 4.8° tilt



Optimized Comb Drive Actuator for Holography

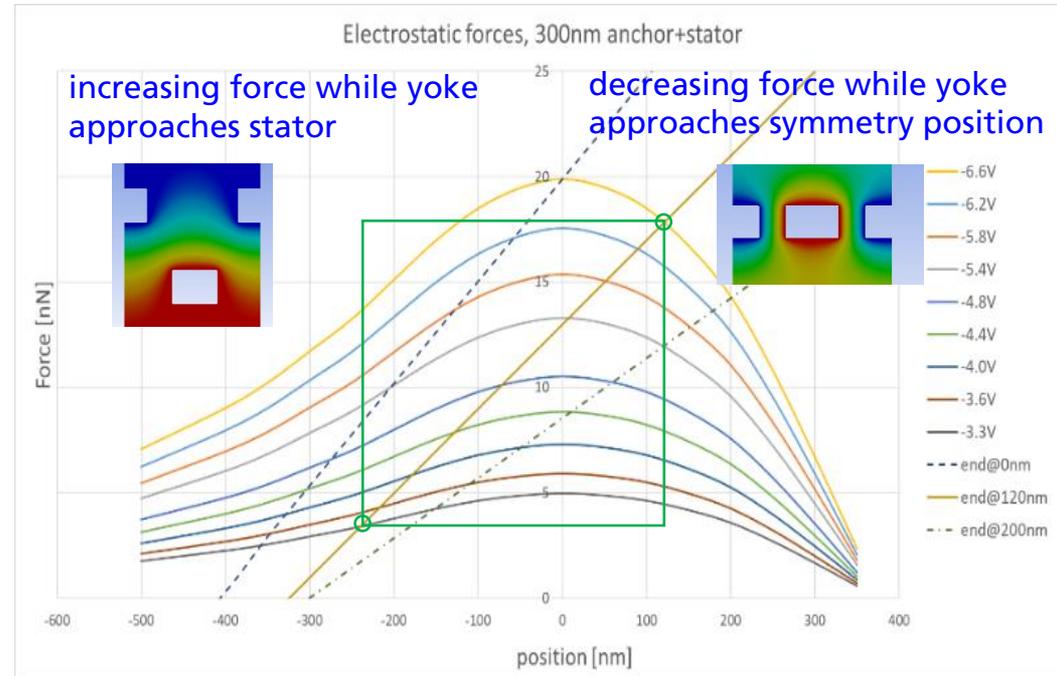
optimized basic concept of the comb drive actuator

- two hinges make for a parallelogram guidance mechanism for tilt suppression
- baseplate, lower hinge, and yoke are on the same electrical potential
→ no charging expected here
- stator, upper hinge and mirror are on the same electrical potential
→ no charging and no cross-talk at mirror edges
- low risk of shortcuts in insulating posts
- for the same total stiffness, each hinge may still be 79% of the thickness of a single hinge



Simulation of Response Curves (I)

- at first only the 3D electrostatic field is simulated for given geometry and a range of actuator positions to get the forces for a fixed voltage
- forces for other cases scale with voltage squared
- two end points for the deflection range may be chosen
- the hinges observe Hooke's law
- from this follow the required spring constant and the zero-voltage vertical gap



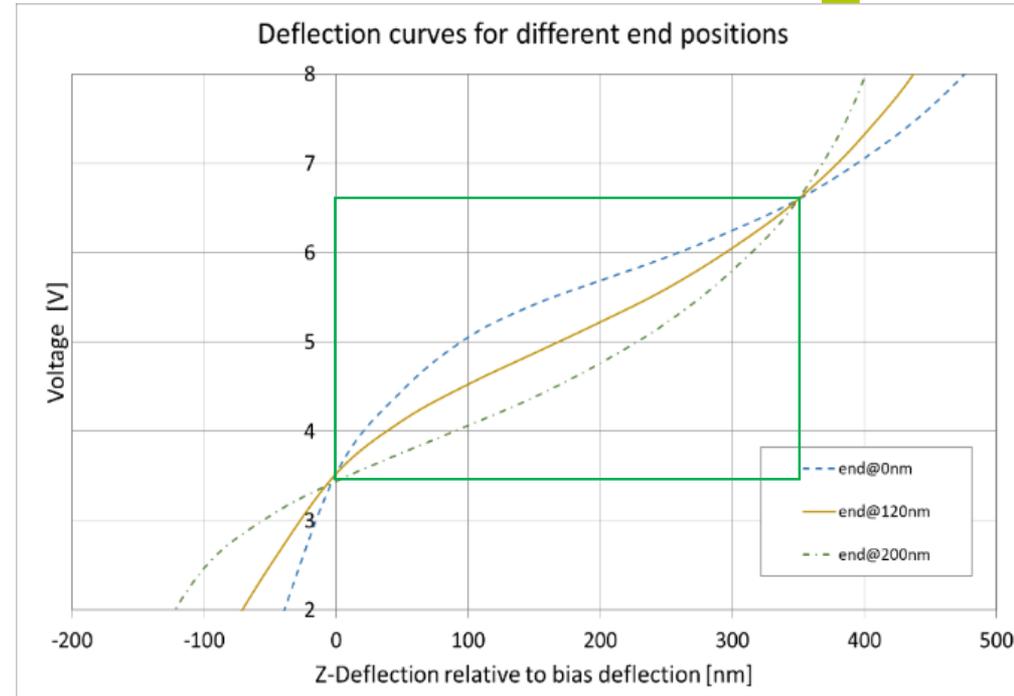
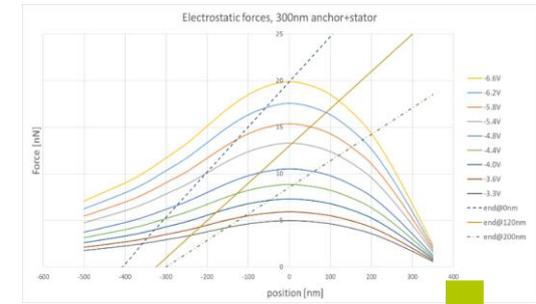
$$k = \frac{F(\text{max. voltage}) - F(\text{bias voltage})}{\text{stroke}}$$

$$\text{zero voltage gap} = \text{gap at bias voltage} - \frac{F(\text{bias voltage})}{k}$$

Simulation of Response Curves (II)

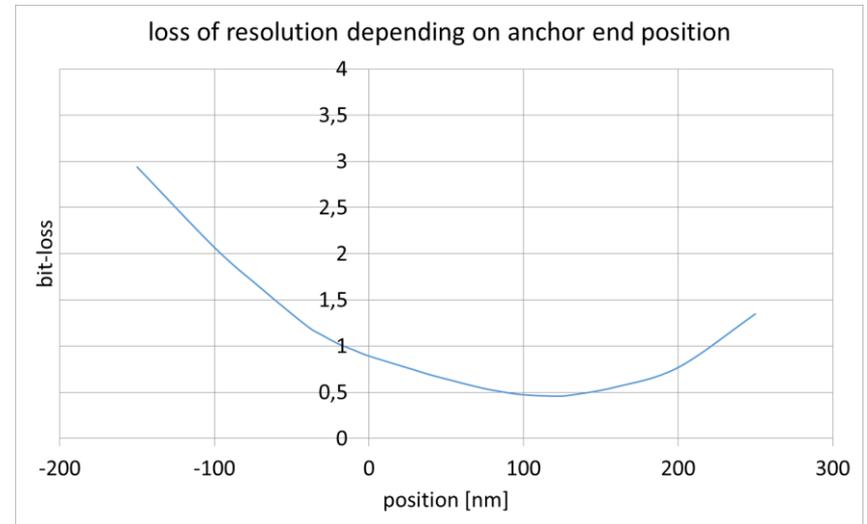
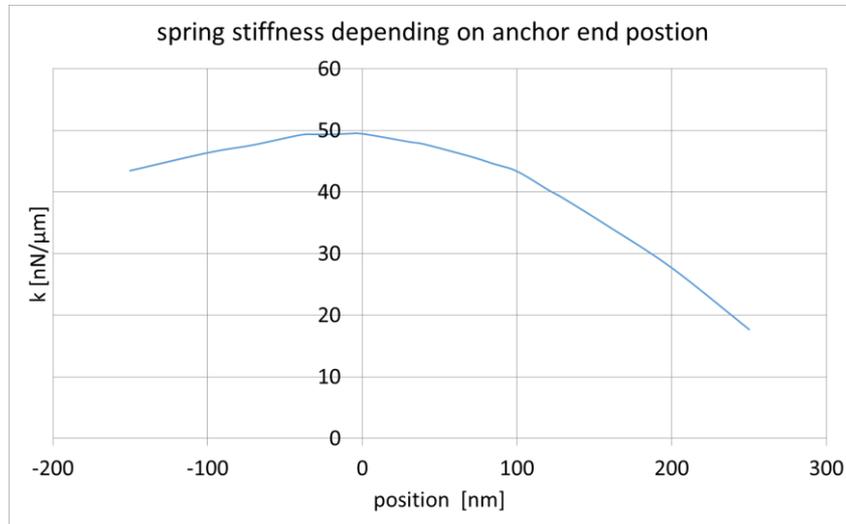
- for each choice of the two deflection range end points (and given geometry of the combs) one gets a response curve from the force equilibrium at each deflection
- the best choice is the response closest to linear
- some choices yield unstable responses
- we evaluate the linearity at the minimum slope (smallest voltage difference for a given deflection change) by:

$$\text{loss of resolution} = \log_2 \left(\frac{\text{average slope}}{\text{minimum slope}} \right) [\text{bit}]$$



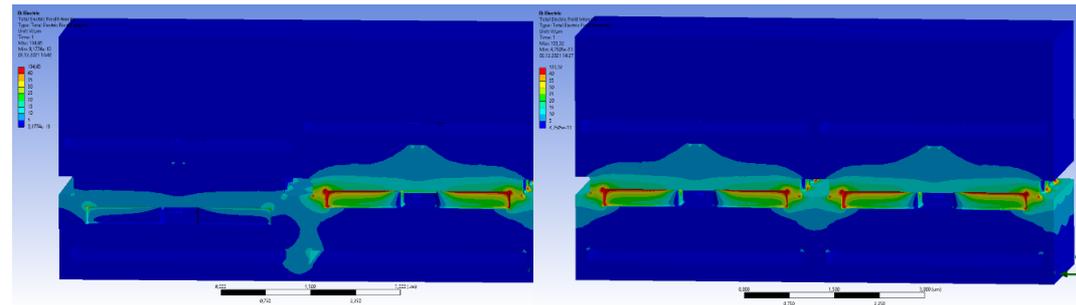
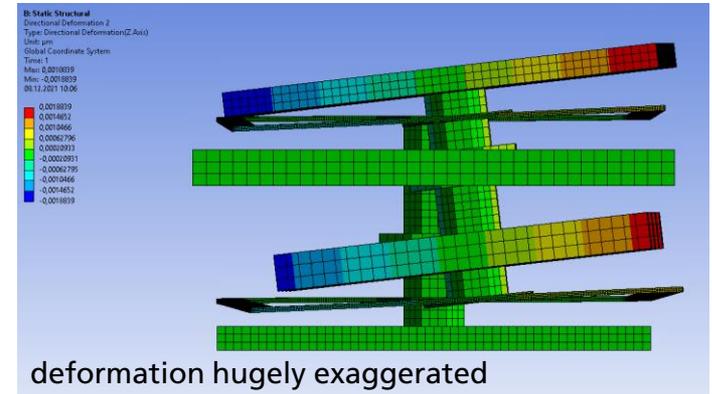
Compromize Choice of Parameters

- we find that an end deflection of about 100nm overlap of the combs yields the best linearity with still near maximum spring constant
- this translates to a 250nm comb separation at bias voltage and about 320nm zero-voltage actuator gap, which is very convenient for manufacturing
- the 'loss of resolution' may be as low as 0.5 bit



First Results on Tilt due to Overlay Errors and Cross Talk

- tilt is found to be within spec limits for overlay errors up to 20nm
- cross talk in the first design is about 0.6%, which is still more than the desired resolution (0.4%)
- this could be ok when compensated by adjusted addressing voltages
- shorter fingers help reduce the cross talk, but they also reduce the total actuator force
- other options for improvement are being investigated



Summary

- Fraunhofer IPMS together with SeeReal and partners is developing an MMA-based SLM optimized for real holographic displays
- the SLM features millions of comb-drive actuators for precise positioning of micro mirrors
- the SLM will exhibit optical properties superior to existing alternatives
- the high quality of the modulated light will allow a natural viewing experience in AR, VR, and MR applications

